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DIVISION-THE AVIATION CORPORATION WILLIAMSPORT, 38, PENNA.

INVESTIGATION OF THE PERFORMANCE OF THE 70727 REED VALVE COMBUSTION CHAMBER USING THE 70862 FUEL SCREEN

Section I - Item 3 - Contract NOa(s)-4718

Best Available Copy

LYCOMING
DIVISION-THE AVIATION CORPORATION

REPORT NO. 1100

PESTRICE

Dates of Test:
February 25, 1947 and
March 5, 1947
Date of Report:
March 31, 1947

INVESTIGATION OF THE PERFORMANCE OF THE 70727 REED VALVE COMBUSTION CHAMBER USING THE 70862 FUEL SCREEN. Section I - Item 3 - Contract NOa(s) 4718

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Navy Dept. (5)

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INVESTIGATION OF THE PERFORMANCE OF THE 70727 REED VALVE COMBUSTION CHAMBER USING THE 70862 FUEL SCREEN.

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APPENDIX

Copies of log sheets, pages 135, 137, 145, 146 are attached to this report.

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PRETER

INVESTIGATION OF THE PERFORMANCE OF THE 70727 REED VALVE COMBUSTION CHAMBER USING THE 70862 FUEL SCREEN.

OBJECT:

1. The object of this investigation was to determine the relative performance of the 70727 reed valve combustion chamber using the 70862 fuel screen.

SUMMARY:

- 2. The 70862 fuel screen is a steel cone with the surface perforated with holes. It was located in the front end of the chamber with the big end toward the rear.
- 3. The 70862 fuel screen was tested in an effort to improve the performance of the 70727 reed valve combustion chamber by promoting better atomization of fuel and mixing with the air.
- 4. The investigation was carried out with both the 1.060° diameter and the 1.375° diameter jet nozzle sizes.
- 5. While use of the 70862 fuel screen promoted steadier operation, no improvement in performance was found.

CONCLUSIONS:

- 6. It is concluded that:
 - (a) Operation with the 70862 fuel screen promotes consecutive sycles more nearly alike, than without the screen.
 - (b) No improvement in performance was found by use of the fuel screen.

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- (c) The performance with the fuel screen was slightly inferior to the "no screen" performance when using the 1.375" jet nozzle. The difference in performance with and without screen when using the 1.06" jet nozzle was negligible.
- (d) Varying the injection nozzle tip distance from the front of the combustion chamber over a range of .75* to 1.75* did not affect performance.

RECOMMENDATIONS:

- 7. It is recommended that:
 - (a) Additional fuel screen and fuel injection nozzle design combinations be submitted for testing.
 - (b) Other methods of introduction of the air-fuel mixture into the combustion chamber be devised for testing.

DESCRIPTION:

- 8. Reference is made to Report No. 1097 entitled "Initial Test of the Multi Reed Valve Combustion Chamber", for a detailed description of the 70727 reed valve combustion chamber.
- 9. Print No. 70862 on page 12 shows the construction of the fuel screen. The sketch on page 5 shows the location of this screen in the combustion chamber.
- 10. A 60° spray angle Bosch injection nozzle was used. METHOD OF TEST:
- 11. Using the 1.360% diameter jet nossle, runs were made 900 cpm, 20 psi ram and about 95 lb/hr fuel flow. Both with and without the fuel screen, three injection nossle tip distances from the front of

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the chamber were tested over a range of .75" to 1.75". This distance (A) is shown on the sketch on page 5.

- 12. Using the 1.375" diameter jet nozzles, runs were made with and without the fuel screen at 900 cpm, 20 psi ram and three fuel flows from about 125 to 190 lb/hr. An injection nozzle tip location of 1.25" from the front of the chamber was used.
- 13. The report referred to in paragraph 8 and also Report No. 1056, entitled "Report on the Initial Test of the Rotary Sleeve Valve Combustion Chamber" describe the test stand and the equipment used in the subject tests.

RESULTS:

- 14. Results of the subject investigation are shown on the curves on pages 6 through 11. Data used is presented on prints of the original data sheets which will be found in the Appendix of this report. In addition, for the runs used, M.I.T. pressure-time indicator cards and photographs of the oscilloscope diagrams taken with the Trimount electronic pressure pick-ups are shown on pages 13 through 26.
- 15. The curve No. 7463, page 6 of thrust versus distance of the injection nozzle tip from the chamber end shows that with or without the use of the fuel screen, thrust remains practically constant over distances of .75" to 1.75" from the chamber end at a given set of operating conditions. This data was taken while using the 1.060" diameter jet nozzle.
- 16. Curves No. 7464 through 7468, pages 7 through 11 show comparative data taken on the 1.375" jet nozzle with and without the fuel screen.

 Over a range of fuel flows, operation without the fuel screen produced both higher thrust and higher specific thrust.

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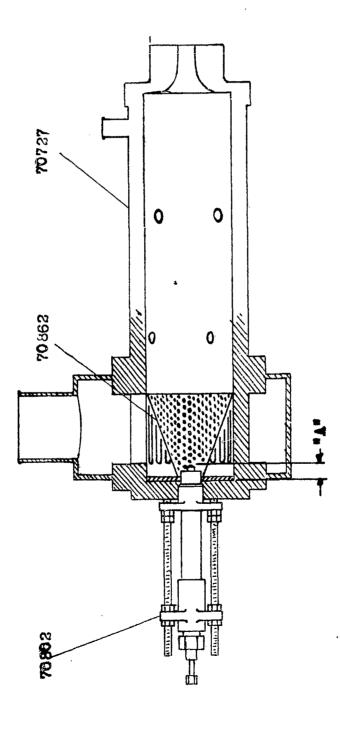
17. Referring to the M.I.T. pressure time indicator cards for run 751 on page 22 and run 754 on page 25, which were taken respectively with and without the fuel screen at the same conditions, it can be seen that the card taken for run 751 has somewhat more scattered points than run 754 because of the unsteadier operation. This condition is more evident when observing the oscilloscope diagrams for runs Nos. 752 and 755 (Page 13) which were taken with and without the fuel screen. DISCUSSION:

18. Tests of the 70862 fuel screens were restricted in scope since 60° was the widest spray angle obtainable with the fuel injection nozzles on hand. It is believed that this angle was too small to cause the fuel to impinge on the fuel screen when in use. To properly evaluate the performance with fuel impinging on the fuel screen in an attempt at better fuel stomization and mixture with the air, the fuel screen and the fuel injection nozzle designs should be selected in combination to ensure that fuel impingement on the screen occurs.

19. Judging by tests so far conducted investigation of other means of introduction of the air fuel mixture into the combustion chamber are imperative if any appreciable operational improvement is to be gained.

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Sketch of 70862 Fuel Screen Installed in the 70727 Reed Valve Combustion Chamber



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FORM-673 26 Pages, PAGE NO. 6 REPORT NO. 1100 REED VALVE COMBUSTION CHAMBER 1060 M. DYA VEY NOEZLE 920 GEN 23 FEN BAN 26 LB/YE F/EL ELOW OFFEOX DATE FREEVARY 25 F99/

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26 Pages, PAGE NO. 9 LYCOMING
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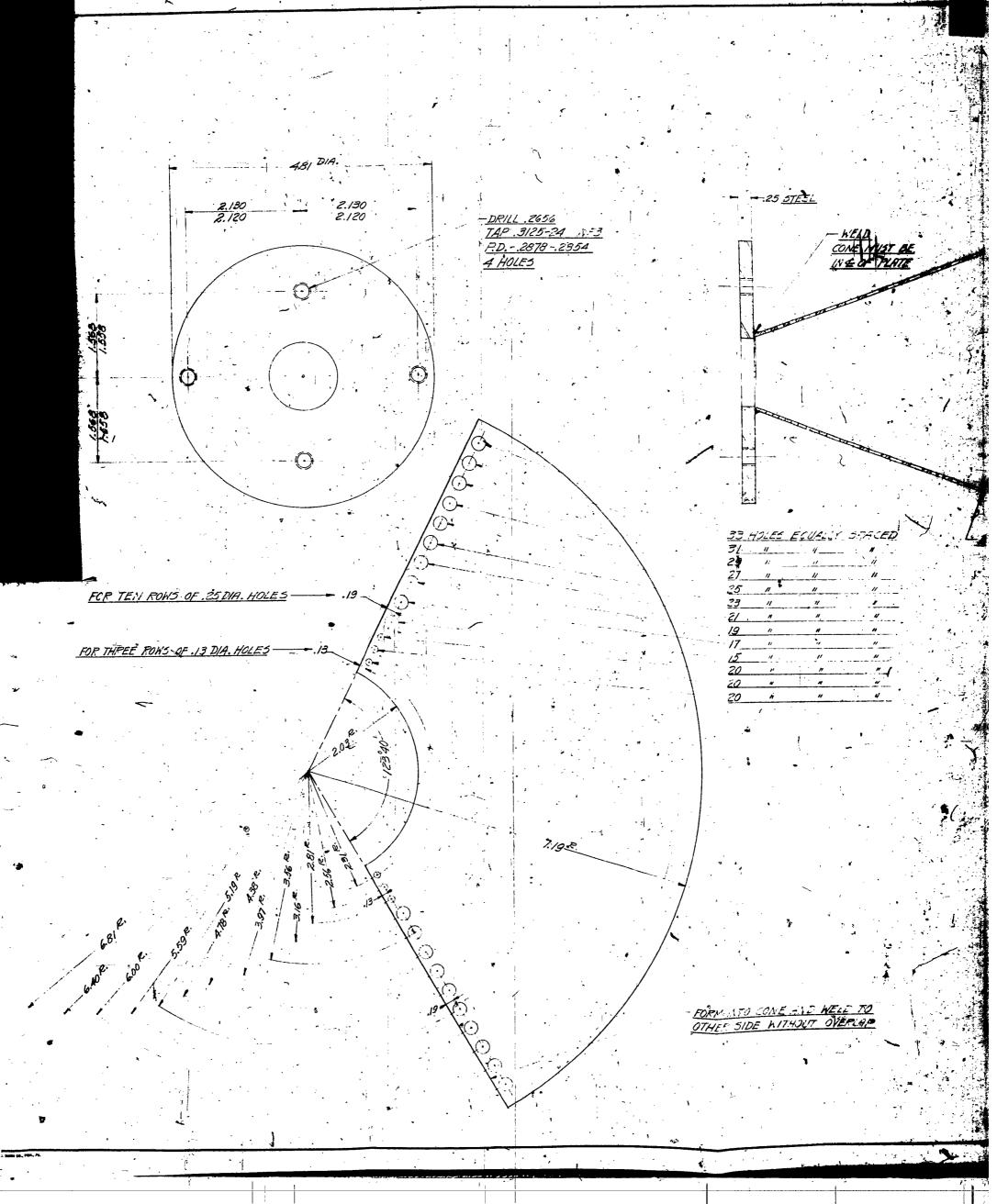
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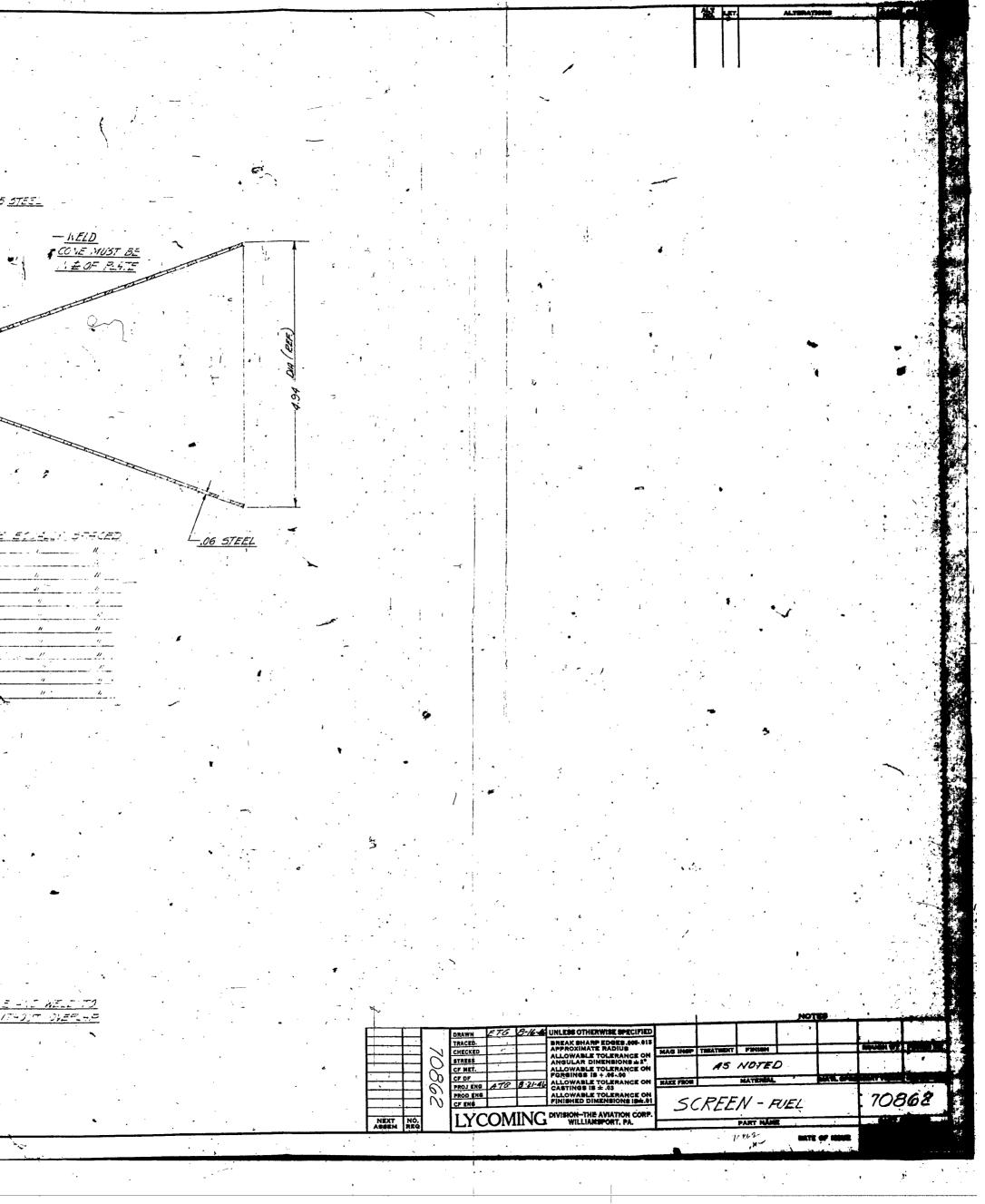
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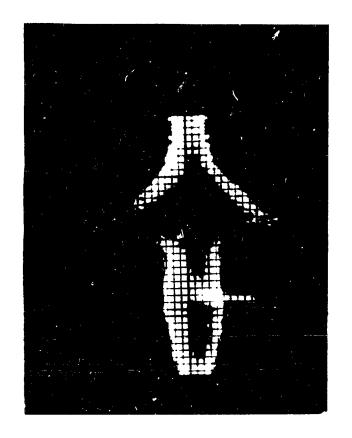
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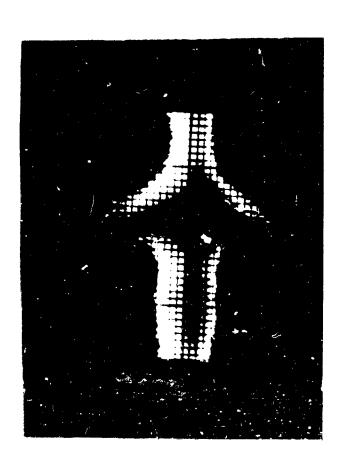
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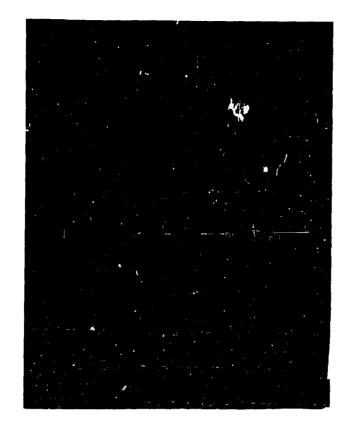








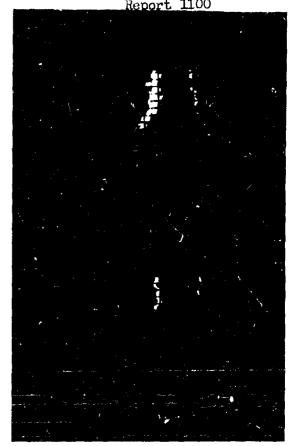
From Left to Right, Run Nos. 752 with Fuel Screen and 755 without Fuel Screen. 1.375" Dia. Jet Nozzle. 900 CPM., 20 PSI Ram. March 5, 1947





From Left to Right, Run Nos. 729 and 730
Fuel Screen In. 1.060" Dia. Jet Nozzle.
Fuel Injection Nozzle Tip .75 and 1.25 Inch
from Front Wall of Chamber.
900 CPM., 20 PSI Ram. February 25, 1947





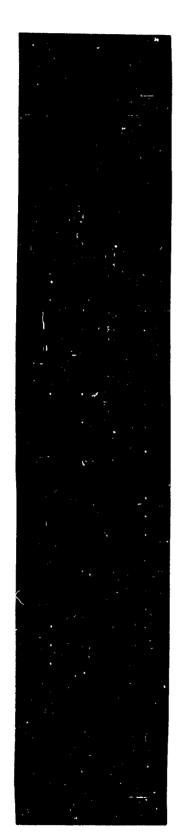


Ebove, from Left to Right, Run Nos. 733 and 734. To the Right, Run No. 735.

Fuel Injection Nozzle Tip .75, 1.25 and 1.75 Inches Respectively from Front Wall of Chamber. No Fuel Screen. 1.060" Dia. Jet Nozzle.

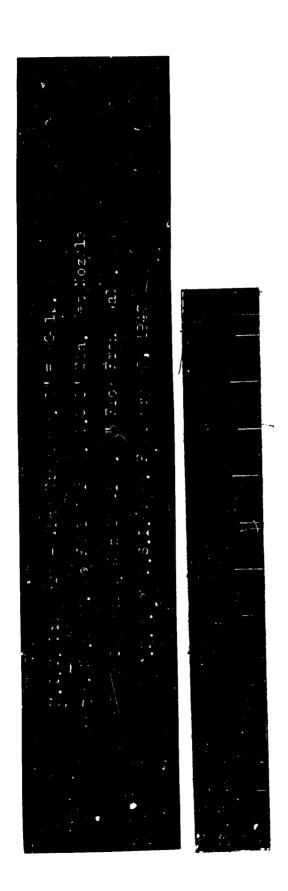
900 GPM, 20 FSI Ram February 25, 1947





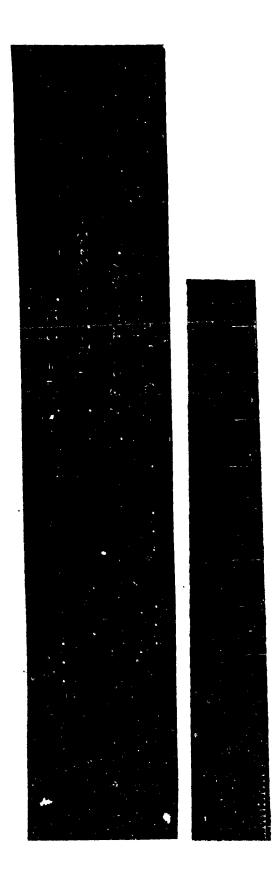


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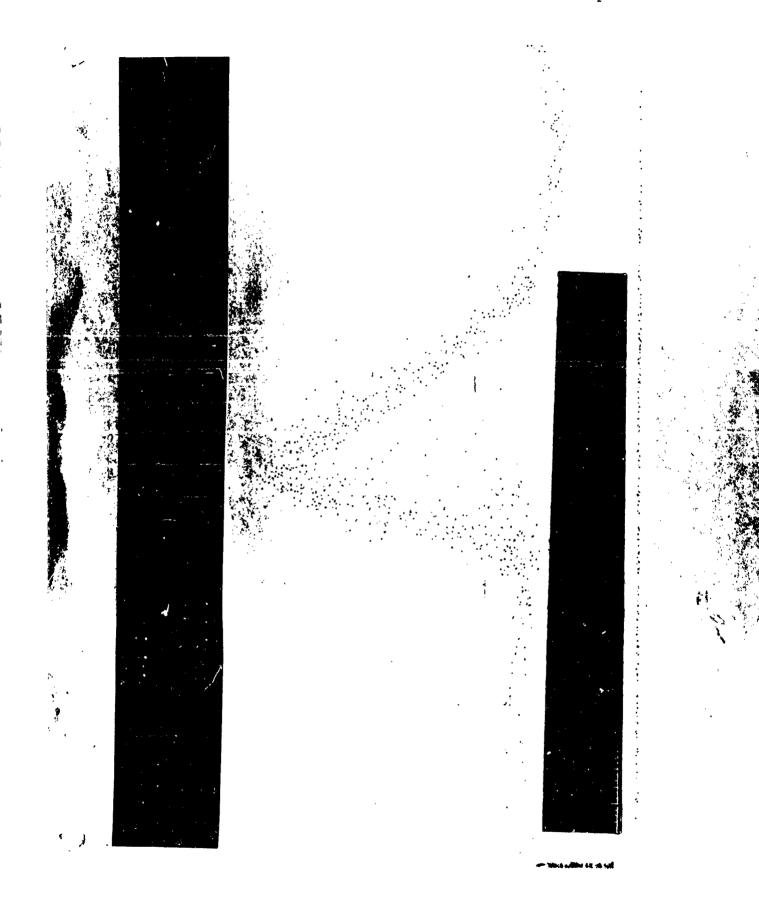
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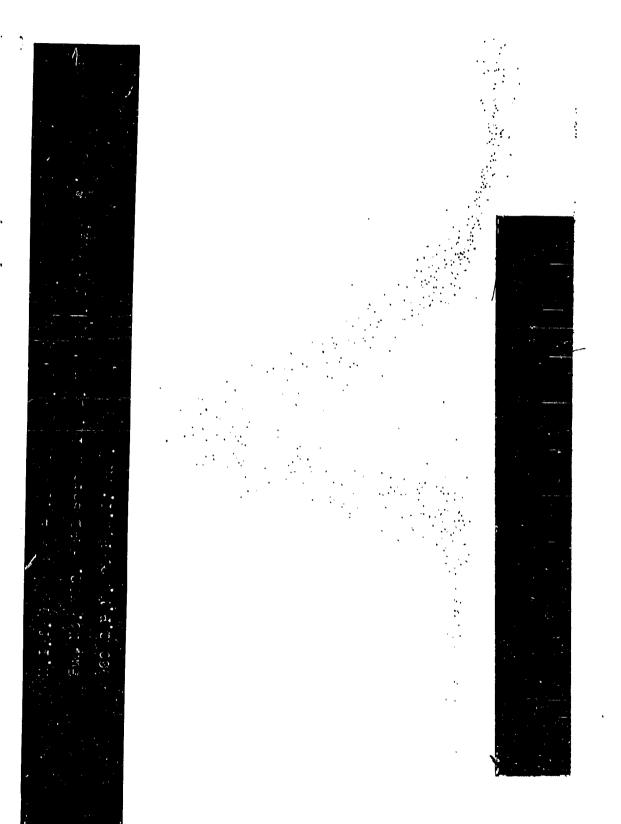
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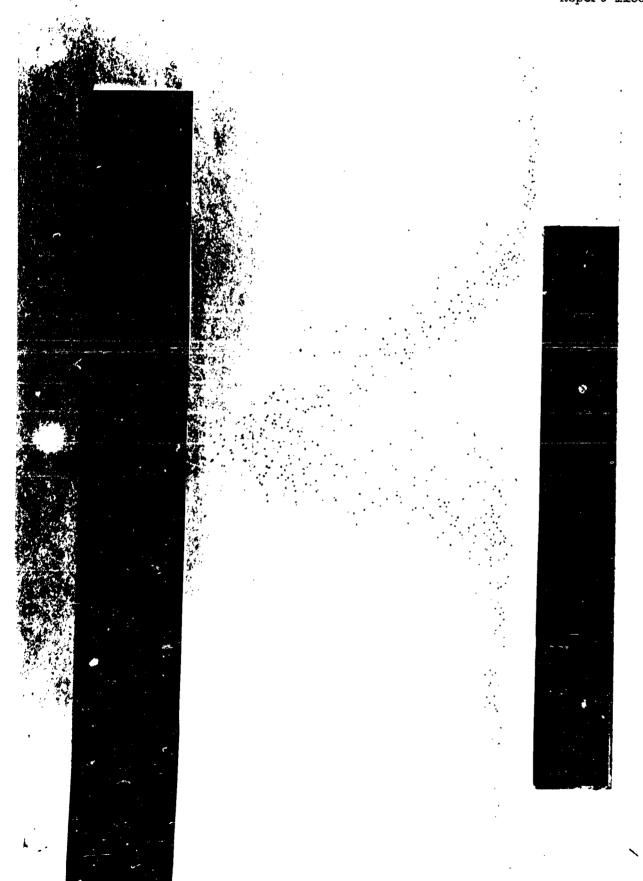
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rest FUEL CASHET IN. AERO PULSE 146 Sheet No /46 Date 3-5-47 DA JET NOTZLE CHEMINED DATE INV NOZZLE /2 IN FROM FROM FRONT FRONT FIRM FROM EULLY KRTRACTED STOP 753 755 RUH NO. SHART SHOP hit In a 3:31 14:20 3160 4:04 4:10 3:5% Time of Day 3:07 3116 903 910 895 896 902 Gyelac Speed TPM 20 20 20 20 Ram All Pressure PSTG 20 20 195 155 195 130 Fuel Flow Meter 10.66 112.86 N 9.00 8:55 Fuel Time Sec Op 40 6 Fuel Temp. 5,930 6,936 #/Ga. 5.930 SA34 Fuel Sp Wh 15 G_{-1} . 4 .5 Fuel Samp. 11.0 59.4 59.0 610 9 PS7 61.0 Throat Caugo Reading 10 Thrust Meter Reading 52.7 44,6 50 52.7 11 Ind. Thrust Hyd Lb Ind Tarust Electron: Lb 21.8 21.8 22.2 Cyl Press -Gauge Read g FSIG 21.8 22,0 340 100 Press Meter Read a 25 24.8 24.3 Tod Cy. 29 28 24.2 PSTG tress Electronic 1400 184,99 1 14A4 I ~ ló Comb arritain PS 76,5 76.5 76.1 Comb Att. Corco 21 20.5 19.4 20.3 19.4 21.2 4 P 18 Comb and their "Hed 153 158 130 147 152 Comb Arr In T, o_R 618 540 612 607 20 Comb 613 ATT L. OW TI 2830 2890 12810 2000 2920 1 21 ARRELOT Lb/Hr 14,0 17.0 "H20 17:0 22 Gooling Later Press 18.5 50 50 23 Coclang Water T O.E. 50 Ţŋ 113 1/0,5 Or 108 100 107.5 Cooling Water T Our. THEY THEY 413 351 .274 25 PS* 332 .261 Districte & Theory of Arms Lo. 0173 .01765 0132 .014 0186 COMIS CAMOUS 1030- 940? 1040 0/3 1060 TEMP loho سيرن RAM ATTR 130 135 TRACK 108 122 130 545 OL 590 540 568 582 1507 190 DISP HESER 126 1150 192.2 RATTO 14.8 43.8 FUE 6 19.16 18.45 14.72 50 35.9 MAN PRESS (MEAN) 36,5 36.0 35.7 35.5 18.8 19.2 18.7 P316 18.8 14.0

LYCOMING

* Reas augs solves - 61 * plause, our consumer day